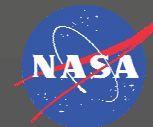


NASA N3-X with Turboelectric Distributed Propulsion

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NASA Glenn Research Center
Cleveland, Ohio

Fundamental Aeronautics Program
Fixed Wing Project

www.nasa.gov



NASA Subsonic Transport System Level Metrics



Strategic Thrusts

1. Energy Efficiency

2. Environmental Compatibility



v2013.1

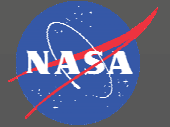
TECHNOLOGY BENEFITS*	TECHNOLOGY GENERATIONS (Technology Readiness Level = 4-6)		
	N+1 (2015)	N+2 (2020**)	N+3 (2025)
Noise (cum margin rel. to Stage 4)	-32 dB	-42 dB	-52 dB
LTO NOx Emissions (rel. to CAEP 6)	-60%	-75%	-80%
Cruise NOx Emissions (rel. to 2005 best in class)	-55%	-70%	-80%
Aircraft Fuel/Energy Consumption† (rel. to 2005 best in class)	-33%	-50%	-60%

* Projected benefits once technologies are matured and implemented by industry. Benefits vary by vehicle size and mission. N+1 and N+3 values are referenced to a 737-800 with CFM56-7B engines, N+2 values are referenced to a 777-200 with GE90 engines

** ERA's time-phased approach includes advancing "long-pole" technologies to TRL 6 by 2015

† CO2 emission benefits dependent on life-cycle CO2e per MJ for fuel and/or energy source used

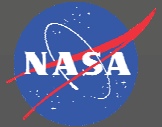
Research addressing revolutionary far-term goals with opportunities for near-term impact



Reference Aircraft – The Boeing 777-200LR

- **Passengers: 300**
- **Payload: 118,000 lbs (53.500 kg)**
- **Range: 7500 nm (14000 km)**
- **Cruise speed: Mach 0.84 @ 35k ft**
- **Fuel: 279,800 lbs (126.900 kg)**



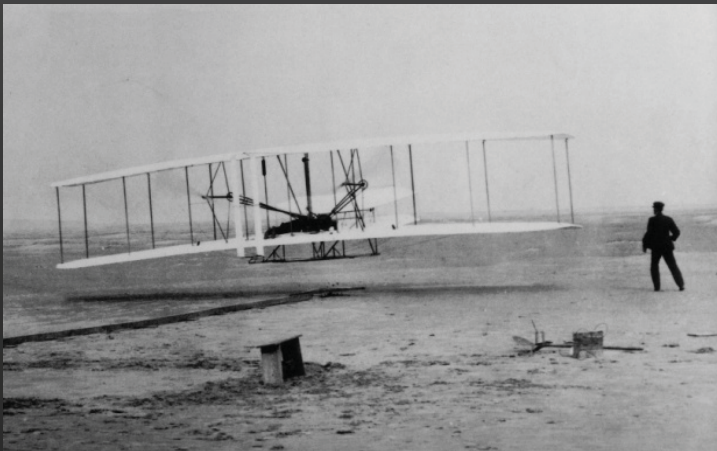
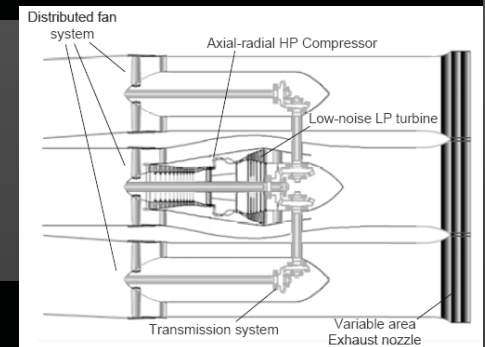


Many Approaches to Distributed Propulsion

Gas-Driven:

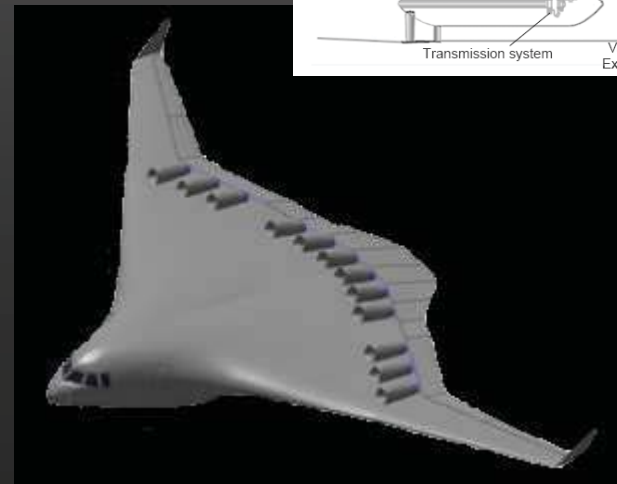


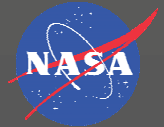
Gear-Driven:



Chain-Driven:

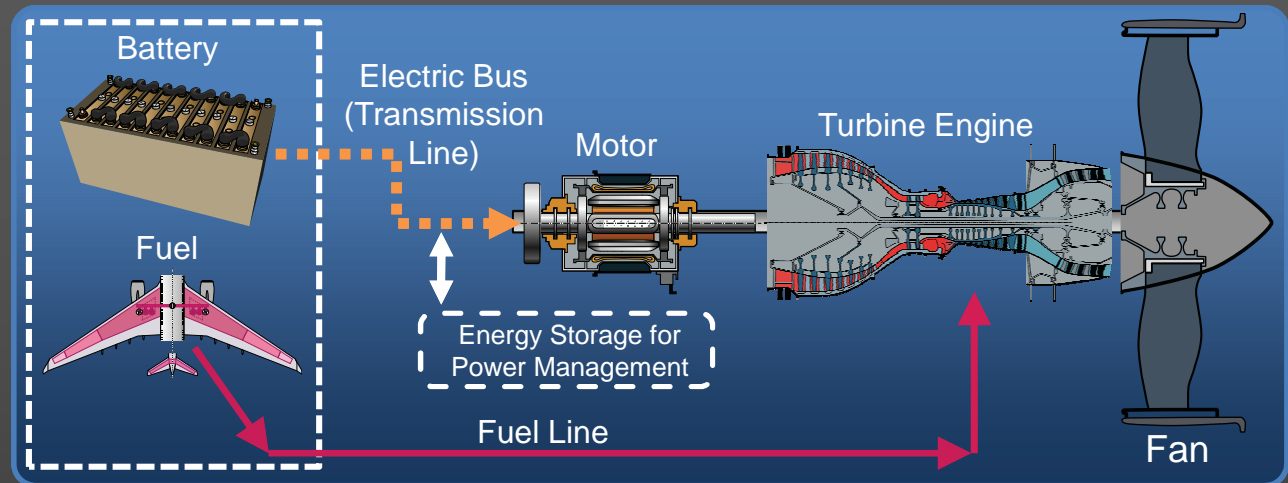
Individual Engines:





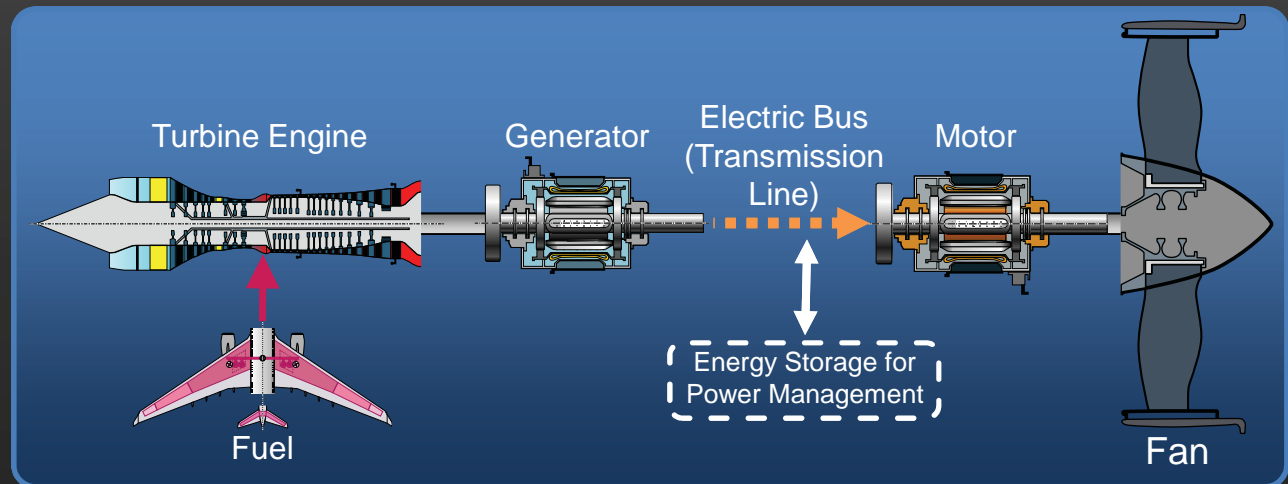
Types of Electric Propulsion

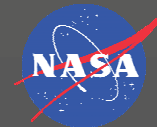
Hybrid Electric



Both concepts can use either non-cryogenic motors or cryogenic superconducting motors.

Turbo Electric





Wide Propulsor
Array Maximizes
Boundary Layer
Ingestion & Wake
Filling

Many Small, Distortion-Tolerant
Fans Yields Large Total Area and
High Effective Bypass Ratio

Superconducting
Motors/Generators

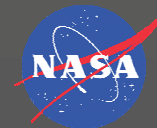
Highly Efficient
Gas Generator

Forward and Aft
Fan Noise Shielding
by Airframe

Superconducting
Redundant DC
microGrid



N3-X
N3-X



N+3 Technology Cycle Design Values

Propulsor

Fan Pressure Ratio	=	1.3
Fan Efficiency	=	95.3% (podded)
	=	94.3% (embedded)
1% embedded distortion efficiency penalty		
Inlet Total Pressure Loss	=	0.2%

Turboshaft Engine

Polytropic Efficiencies:

LPC/HPC	=	0.9325
LPT/HPT	=	0.93
PT	=	0.924

Temperature Limits:

T3	=	1810 R (1006 K)
T4	=	3360 R (1867 K)

Cooling (*Uncooled CMC rotors/stators*):

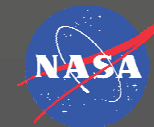
HPT	=	4% (nonchargeable)
LPT	=	2% (nonchargeable)
PT	=	1% (chargeable)

Electrical System (N3-X/TeDP)

BSCCO	Motor Eff	=	99.94%
	Generator Eff	=	99.93%
	Tmax	=	50 K
MgB2	Motor Eff	=	99.97%
	Generator Eff	=	99.98%
	Tmax	=	30 K
Inverter	Efficiency	=	99.93%
	Tmax	=	100 K
Cryocooler % of Carnot Eff	=	30%	
	Tsink	=	Tamb

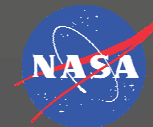


TeDP Cycle Results



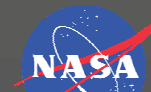
	RTO		TOC	
	BSCCO	MgB ₂	BSCCO	MgB ₂
Total Vehicle Thrust - lbf	94,200	85,800	35,500	33,400
Specific Fuel Consumption - lbf/hr/lbf	0.236	0.217	0.341	0.313
Specific Energy Consumption - BTU/s/lbf	1.216	1.194	1.761	1.727
Effective bypass ratio	35	36	29	30
Overall pressure ratio	57	57	84	84
Max compressor exit temperature - °R	1,800	1,800	1,680	1,680
Maximum turbine inlet temperature - °R	3,360	3,360	3,260	3,260
Fan nozzle exit velocity - ft/s	610	600	990	990
Turboshaft nozzle exit velocity - ft/s	760	750	1,370	1,360
<i>RTO (sea level, M0.24, ISA+27 °R)</i>		<i>TOC (34,000 ft, M0.84, ISA)</i>		

Electrical System

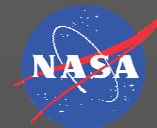


		BSCCO	MgB ₂
Generator X 2	Power – hp (MW)	41080 (30,6)	37840 (28,2)
	Power/Weight – hp/lb (kw/kg)	35 (57)	35 (57)
	Weight – lbs (kg)	1180 (536)	1090 (494)
Motor X 14	Power – hp (MW)	5920 (4,42)	5280 (3,94)
	Power/Weight – hp/lb (kw/kg)	14 (23)	14 (23)
	Weight – lbs (kg)	410 (186)	365 (166)
Inverter X 14	Power/Weight – hp/lb (kw/kg)	18 (30)	18 (30)
	Weight – lbs (kg)	323 (147)	299 (136)
Cooling System	Total Cryocooler Wt – lbs (kg)	5130 (2327)	
	LH2 Tank Wt – lbs (kg)		1510 (685)
Grid	Cable + Protection – lbs (kg)	3570 (1619)	3290 (1492)

Propulsion System Weight



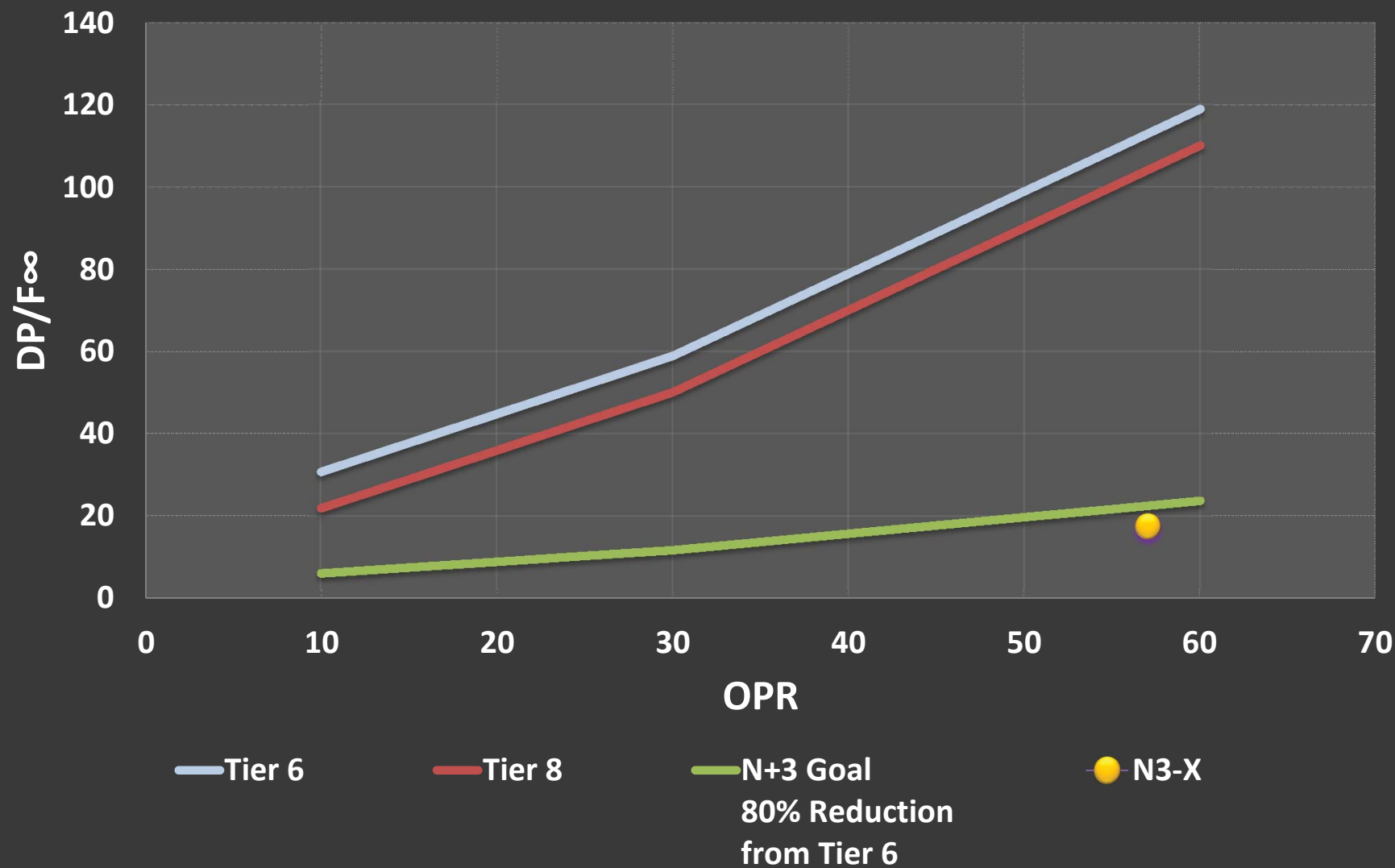
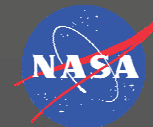
		BSCCO	MgB ₂
Turbogenerator	Turboshaft Engine & Nacelle – lbs (kg)	4310 (1955)	4070 (1846)
	Generator – lbs (kg)	1180 (535)	1090 (494)
	One Turbogenerator – lbs (kg)	5491 (2491)	5157 (2339)
Propulsor	Fan + Nacelle – lbs (kg)	1562 (709)	1424 (646)
	Motor + Inverter – lbs (kg)	733 (332)	664 (301)
	One Propulsor – lbs (kg)	2295 (1041)	2088 (947)
Cooling System	Total Cryocooler Wt – lbs (kg)	5130 (2327)	
	LH2 Tank Wt – lbs (kg)		1510 (685)
Grid	Cable + Protection – lbs (kg)	3570 (1619)	3290 (1492)
Total System	2 TurboGen + 14 Props + Cooling + Grid	51,820 (23.505)	44,335 (20.110)
777-200LR	2 GE90-115 "Dry" + Nacelle + Pylon	47,300 (21.455)	

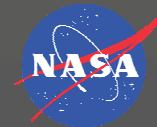


Mission Fuel/Energy Consumption

		Weight lbs (kg)	Mission Fuel Consumption lbs (kg)	Mission Energy Consumption BTU(MJ)	Mission Energy Reduction
	777-200LR Class Aircraft	768,000 (348.400)	280,000 (127.000)	5.2E+09 (5.5E+06)	
	N3-X BSCCO/Cryocooler	515,000 (233.600)	85,000 (38.560)	1.6E+09 (1.67E+06)	70%
	N3-X MgB₂/LH₂	496,000 (229.800)	76,000 (34.470)	1.5E+09 (1.55E+06)	72%

N3-X LTO NOx Comparison





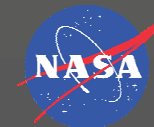
- Exposed Turboshaft Engine
 - Primary Noise Source
 - Inadequate nozzle length for Noise Treatment
- Flush Vectoring Propulsor Nozzle
 - Eliminates Scrubbing Noise
 - Aft Fan Noise Much Smaller Than Turbomachinery and Approach Flap Noise

• **Estimated 32 EPNdB Cum Below Chapter 4**



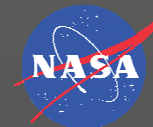
- Buried Turboshaft Engine
 - Moved to wing root
 - Leading Edge S-Duct Inlet
 - Upper Wing Surface Exhaust
- Setback Propulsor Nozzle
 - Eliminate Vectoring Nozzle at Price of Some Scrubbing Noise
- Low-noise Slotless Flaperons

• **Estimated 64 EPNdB Cum Below Chapter 4**



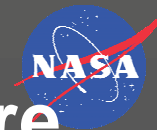
Comparison of N3-X to FW Metrics

Metric	N+3 Goal	N3-X
Noise (Cum Margin Rel to Chapter 4)	-52 db	-32db/-64 db
LTO NOx Emissions (Rel to CAEP Tier 6)	-80%	-85%
Cruise NOx (Relative to 2005 best in class)	-80%	
Aircraft Fuel/Energy Consumption (Relative to 2005 Best In Class)	-60%	-70% / -72%

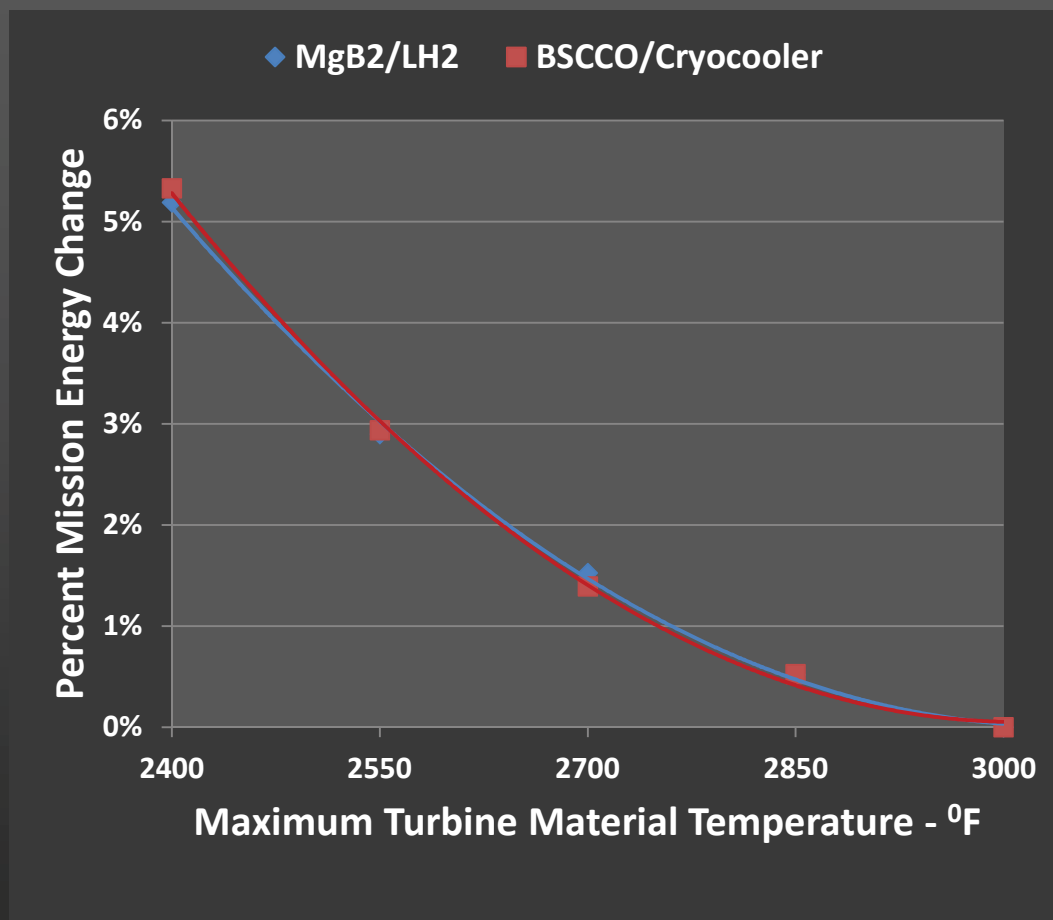


Mission Energy Sensitivity to Propulsion System Parameters

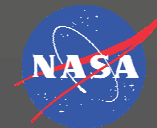
Parameter	Change	Mission Energy Sensitivity
TSFC	+1.15%	+1.0%
Propulsion System Weight	+10%	+0.8%
Inlet Total Pressure Loss	+1.0%	+3.0%
Fan Efficiency	+1.0%	+1.0%
Fan Pressure Ratio	+0.05	+2.0%
Compressor Discharge Temp	-50 °R	+1.0%
LPC Polytropic Efficiency	-1.0%	+0.81%
HPC Polytropic Efficiency	-1.0%	+0.43%
HPT Polytropic Efficiency	-1.0%	+0.72%
LPT Polytropic Efficiency	-1.0%	+0.43%
PT Polytropic Efficiency	-1.0%	+0.27%



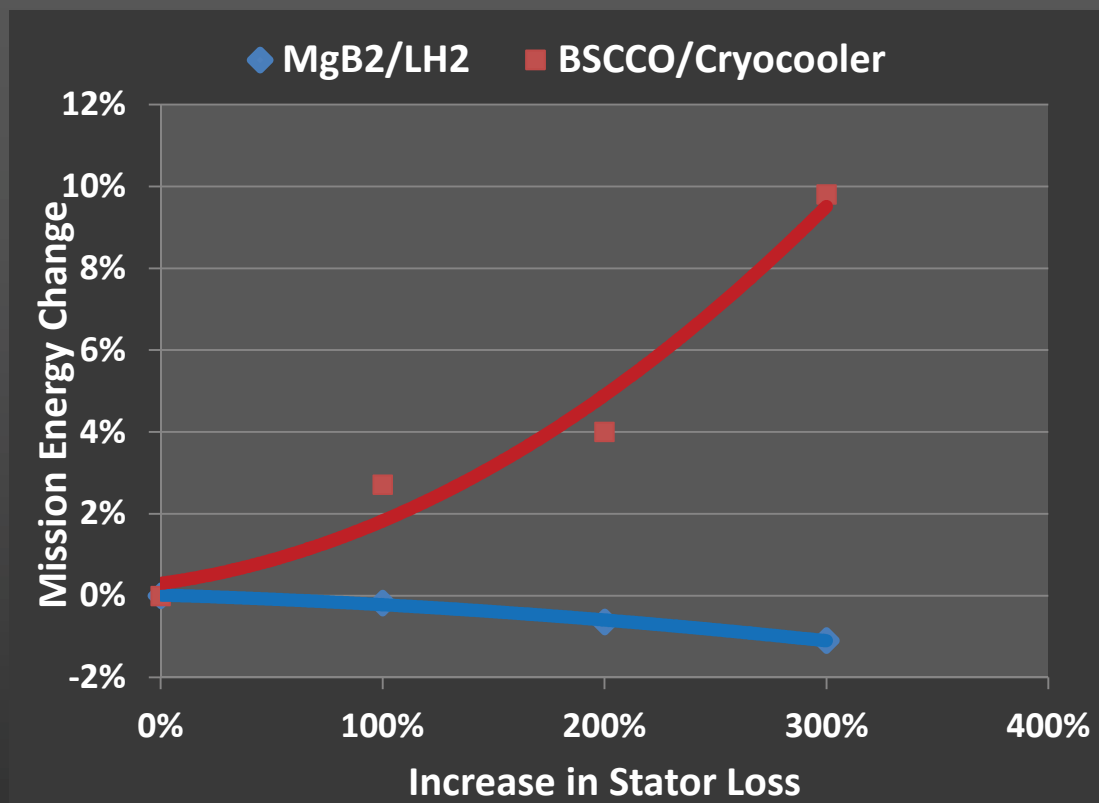
Sensitivity to Turbine Rotor Inlet Temperature



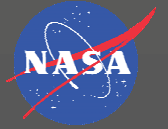
- Current SOA CMC Temperature Limit is 2400 °F
- Technology development roadmap to get to 2700 °F has been defined
- **300 °F reduction from baseline only increases mission energy by 1.5%**
- Using cooled metallic blades for the HPT rotor one blades could allow TIT to remain at 3000 °F with CMC in subsequent rotors



Sensitivity to Stator Loss



- Stator Loss Effected By Superconducting Filament Size
- Assumed 10 micron
- SOA is 40-50 micron which results in 200% higher loss
- Addition loss in BSCCO/Cryocooler results in increased cryocooler size and power yielding 4% increase in mission energy
- **Counterintuitively MgB2/LH2 Mission Energy DECREASES with increasing stator loss.**
- This is due to more LH2 required for cooling which REDUCES total fuel weight which reduces mission energy



Questions?

